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SPEED-ENHANCEMENT OF NEUTRON YIELD

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ABSTRACT: Removing the speed limitation of present generation plasma focus devices would improve the present scaling law of $Y \sim I^4$ to an ultimate $Y \sim I^8$. Speed-enhanced experiments are planned.

1. INTRODUCTION

The plasma focus PF is important for generating fusion neutrons. An analysis of data for PF devices in their wide range of sizes from 1 kJ (small) to 1 MJ (large) shows the following **experimentally** observed features: (1) They follow the neutron yield Y scaling law with focus current I of $Y \sim I^4$ and (2) For neutron optimized operation they all (a) have the same limited axial speed v_a of 10 cm/ μ s and radial on-axis collapse speed v_r of 25 cm/ μ s driven by a standard value of undamped current per unit anode radius $I_0/a = 250$ kA/cm (b) operate in a narrow range of pressures of several torr (D_2).

In this paper we propose that removing the speed limitation would result ultimately in a **vastly improved scaling of $Y \sim I^8$** which could enhance prospects of the PF as a fusion contender. We deduce the speed-enhanced scaling law as follows: First consider the thermonuclear component Y_{th} of the yield.

2. THERMONUCLEAR COMPONENT OF YIELD, Y_{th}

Operating in deuterium

$$Y_{th} = \frac{1}{2} n_f^2 \langle \sigma v \rangle (r_f^2 z_f) \tau_f \quad (1)$$

n_f = PF number density. Radius r_f , length z_f (Lee 1983), lifetime τ_f of the PF column are each $\sim a$, the anode radius. We thus write:

$$r_f = a k_f \quad (2) \quad z_f = a(1-k_f) = 0.88a \quad (3)$$

where $k_f = r_f/a$ = radius ratio of 0.12 for the deuterium focus and

$$\tau_f = \frac{a}{c_1 (I_f/a) / \rho_0^{1/2}} \quad (4)$$

f_{en} = observed lifetime enhancement factor, μ = permeability and

$$\text{where } c_1 = \frac{\sqrt{\mu}}{2\pi f_{en} d_f} \left[(1/k_f)^2 + \frac{\gamma f_{Is}}{2} \right]^{1/2}$$

f_n = reflected shock over-pressure ratio (Lee 1988). PF radial speed v_f (Lee et al 1988, Lee 1990) is proportional to the current linear density (as is the axial speed):

$$v_f = \frac{I_f/a}{\rho_o^{1/2}} c_2 \quad (5) \quad \text{where } c_2 = \frac{\mu^{1/2} (1+\gamma)^{1/2}}{4\pi k_f}$$

$$\text{Hence } a = \frac{I_f}{v_f \rho_o^{1/2}} c_2 \quad (6)$$

Putting Eqs 2-6 into Eq 1 we have

$$Y_{th} = c_x \frac{I_f^4}{v_f^5} \langle \sigma v \rangle \quad (7)$$

$$\text{where } c_x = \frac{1}{2} (n_f/\rho_o)^2 k_f^2 (1-k_f) c_2^5 / c_1$$

From nuclear data (Glasstone & Lovberg 1960) we may fit, in the range 1 - 5 keV, for the deuterium fusion reaction:

$$\langle \sigma v \rangle_{D-D} = c_N T^{4.5} \quad (8)$$

where c_N = constant. From pressure balance we write the focus temperature T_f (Lee 1983) as:

$$T_f = c_3 \frac{(I_f/a)^2}{\rho_o} = c_4 v_f^2 \quad (9)$$

$$\text{where } c_4 = \frac{\mu}{4\pi^2} \frac{m}{k(1+Z)} f_{Is} / c_2^2$$

where m = mass of deuterium atom, k = Boltzmann constant and Z =charge. Put Eq 9 into Eq 8 and then Eq 8 into Eq 7 and we have:

$$Y_{th} = c_y I_f^4 v_f^4 \quad (10)$$

where $c_y = c_x c_N c_4^{4.5}$. We note that c_y may be taken to be constant over the range of PF devices. From (10) it is seen that Y_{th} scales as I^4 since v_f is practically a constant in existing PF devices.

3. BEAM TARGET COMPONENT OF YIELD, Y_{bg}

Next we consider the beam-gas component Y_{bg} . We write:

$$Y_{bg} = n_o \int N_b \sigma(x) dx \approx n_o N_b \sigma L \quad (11)$$

where n_o is number density of target gas, N_b is total number of ions in the beam and $\sigma(x)$ is the fusion cross section, and σL represents the product of cross section and effective interaction length. From available nuclear data we may write

$$\sigma L = c_5 E_b^{3/2} \quad (12)$$

where E_b is the beam energy in the range 100 - 1000 keV. Assuming an inductive model for the beam energy we have

$$E_b = c_6 v_f I_f \quad (13)$$

We assume N_b depends on the number of particles in the plasma focus volume we write

$$N_b = c_7 a^3 \rho_o = c_8 \frac{I_f^3}{v_f^3 \rho_o^{1/2}} \quad (14)$$

where $c_8 = c_7 c_2^3 (1 - k_f)$. Combining Eqs 11 - 14 we have

$$Y_{b-g} = c_z \frac{I_f^{4.5} \rho_o^{1/2}}{v_f^{3/2}} \quad (15)$$

where $c_z = c_5 c_6^{3/2} c_8 n_o / \rho_o$. Here c_z may be taken as constant. Eq 15 shows that $Y_{b-g} \sim I^{4.5}$ for operation at fixed density and v_f .

4. NEUTRON YIELD Y

The total neutron yield is $Y = Y_{th} + Y_{b-g}$ and Moo et al (1991) have shown that $Y_{b-g}:Y_{th}$ is of the order of 85:15. Thus Equations (10) and (15) are not inconsistent with the observed neutron yield scaling law of $Y \sim I^4$, noting that this scaling law is at best an indicative one based on many experiments conducted under diverse conditions.

5. SPEED-ENHANCEMENT FOR YIELD $Y \sim I^8$

Equations (10) and (15) also indicate that if experiments do not limit the speed of operation, then $Y_{th} \sim I^4 v_f^4$ will increase above the I^4 scaling whilst $Y_{b-g} \sim I^{4.5}/v_f^{1.5}$ will have a scaling law poorer than $Y_{b-g} \sim I^{4.5}$. In the limit keeping 'a' constant whilst increasing I , Eq (5) indicates $v_f \sim I$ so that in that limit (constant 'a'):

$$Y_{th} \sim I^8 \quad \text{and} \quad Y_{bg} \sim I^3$$

From the above analysis the following conclusions are drawn:

Operation at increased speed (above axial speed of 10 cm/ μ s) should: (1) increase Y_{th} preferentially to Y_{bg} and (2) make the scaling law more favourable than $Y \sim I^4$ with the most favourable scaling law being $Y \sim I^8$.

6. SPEED-ENHANCEMENT EXPERIMENTS

Following Mather's pioneering work (Mather 1965) it appears that all Mather-type plasma focus devices, big and small, have been designed for optimum operation around a standard value of $I_0/a = 250$ kA/cm. Experiments have shown that when pressure is varied good focusing is observed only in the limited axial speed range of 6 - 10 cm/ μ s (Lee 1990). The lower limit is easily understood in terms of poor coupling of the magnetic piston MP with the driven plasma layer, indicated by a low magnetic Reynolds Number R_m (Lee et al 1991), or in terms of low specific energy (Pouzo et al 1988). For the higher speed limit, it appears that the high R_m leads to an effective separation (Lee 1990) of MP from the driven plasma layer. The plasma layer then collapses radially whilst MP is still driving axially. Such a large separation is not conducive to an intense focus.

We propose to limit this force field, flow field separation by a stepped anode structure. The first part of the axial phase uses a regular anode designed for standard $I_0/a = 250$ kA/cm, but shorter than required to match the discharge peak. The regular anode is attached to a stepped-down anode of smaller radius to increase the speed (see Eq 5). This speed-enhanced section should be long enough to increase the speed significantly above 10 cm/ μ s, but short enough to limit force field, flow field separation. Other factors that need to be considered include the mean free path which increases with temperature. Also a fast rise current may enable the use of a shorter anode thus reducing separation. Experiments are designed and results will be reported shortly.

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